Status of Research on Fusion Energy and Plasma Turbulence

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> University of Ottawa Physics Dept. Seminar Nov. 29, 2007

Acknowledgments:

Center for Multiscale Plasma Dynamics <u>http://www.cmpd.umd.edu</u>

 & Plasma Microturbulence Project http://fusion.gat.com/theory/pmp (General Atomics, U. Maryland, LLNL, PPPL, U. Colorado, UCLA, U. Texas) DOE Scientific Discovery Through Advanced Computing

GYRO Simulation movies from:

J. Candy, R. Waltz (General Atomics) <u>http://fusion.gat.com/theory/Gyro</u>

W. Dorland (Maryland), S. Cowley (UCLA), M. Kotschenreuther (U. Texas) W. Nevins (LLNL)

R. Goldston, R. Nazikian, D. Meade, E. Synakowski, D. Stotler, M. Zarnstorff (PPPL) J. Ongena (JET)

The Plasma Microturbulence Project

- A DOE, Office of Fusion Energy Sciences, SciDAC (Scientific Discovery Through Advanced Computing) project (~2001-2004)
- devoted to studying plasma microturbulence through direct numerical simulation
- National Team (& four codes):
 - GA (Waltz, Candy)
 - U. MD (Dorland)
 - U. CO (Parker, Chen)
 - UCLA (Lebeouf, Decyk)
 - LLNL (Nevins P.I., Cohen, Dimits)
 - PPPL (Lee, Lewandowski, Ethier, Rewoldt, Hammett, ...)
 - UCI (Lin)
- They've done all the hard work ...















Plasma self-heating



Electricity Hydrogen



Magnetic Fusion Power System



Two Approaches to Fusion Power Each has R&D Paths with Plausible Technologies leading to Attractive & Economical Energy

- Inertial Fusion Energy (IFE)
 - Fast implosion of high-density D-T fuel capsules.

Reaches ~ 200 Gbar from 25-35 fold radial convergence.

- Several ~ 350 MJ (0.1 ton TNT) explosions per second.
- Magnetic Fusion Energy (MFE)
 - Strong magnetic pressure (100's atm) confine low-density (10's atm) plasma.
 - Particles confined within "toroidal magnetic bottle" for at least ~ 10 km and 100's of collisions per fusion event.
 - Fusion power density (~10 MW/m³ and 20,000 × solar) allows plasma to be sustained for continuous power.

Three Types of Fusion Power



R (m)

The fundamental physics of direct- and indirect-drive ICF implosions is the same



There are two principal approaches to compression in Inertial Confinement Fusion





The 1.8-MJ National Ignition Facility (NIF) will demonstrate ICF ignition and modest energy gain



OMEGA experiments are integral to an ignition demonstration on the NIF.

TC4680m





- Toroidal magnetic chamber
- Steady state, Nb₃Sn magnets^L
 (Coldest ↔ Hottest)
- SiC blanket (~ 1,100 C) with PbLi coolant yields high thermal efficiency.
- Modular, "easy" to maintain, with 85% availability
- I GWe

Blanket Superconducting Magnet

11 m

Fusion's Materials Challenge

- Unlike fission, the by-products of fusion are not inherently radioactive. Fusion has low proliferation risks.
- When fabricated from low activation materials, fusion does not produce long-lived radioactive waste.
- Fusion's materials challenge is to develop long-life, high-strength materials with high neutron-irradiated fracture toughness and good helium swelling resistance.
- Good options exist: Ferritic/martensitic steels, Vanadium alloys, and SiC/SiC composites

Fusion Power
$$\propto n_{\rm D}n_{\rm T} \langle \nabla V \rangle V 17.6 \text{ MeV}$$

 $\propto n^2 T^2$
 $\propto p^2 \propto \beta^2 B^4$

Key performance par ameter:

$$\beta = \frac{plasma \ pressure}{magnetic} = \frac{p}{B^2/8\pi}$$

Lawson Power Balance Criterion
(Simplified)
Key ratio : Fusion Power
Heating Power needed to sustain Plasma

$$= \frac{n^{2} T^{2} T}{\left(\frac{3}{2} \frac{\sqrt{hT} T}{T_{E}}\right)} \propto nTTE$$

$$Q = \frac{Output Fusion Power}{Input Power to Heat Plasma} \approx \frac{5}{\left(\frac{C}{nT} \frac{C}{T_{E}} - 1\right)}$$



Progress in Fusion Energy has Outpaced Computer Speed



Some of the progress in computer speed can be attributed to plasma science.

The Estimated Development Cost for Fusion Energy is Essentially Unchanged since 1980





On budget, if not on time.

\$30B development cost tiny compared to >\$100 Trillion energy needs of 21st century and potential costs of global warming. Still 40:1 payoff after discounting 50+ years.

Fusion can be an Attractive Domestic Energy Source

- Abundant fuel, available to all nations
 - Deuterium and lithium easily available for thousands of years
- Environmental advantages
 - No carbon emissions, short-lived radioactivity
- Can't blow up, resistant to terrorist attack
 - Less than a minute's worth of fuel in the chamber
- Low risk of nuclear materials proliferation
 - No fissile or fertile materials required
- Compact relative to solar, wind and biomass
 - Modest land usage
- Not subject to daily, seasonal or regional weather variation, no requirement for local CO₂ sequestration.
 - Not limited in its contribution by need for large-scale energy storage or extreme-distance transmission
- Cost of power estimated similar to coal, fission
- Can produce electricity and hydrogen
 - Complements other nearer-term energy sources

Comparison of Fission and Fusion Radioactivity After Shutdown



Year After Shutdown

The Value of Fusion-Produced Energy is 12,000x Greater than the Development Cost

Return on investment still ~40:1 payoff after discounting for Net Present Value, 20% advantage over other energy sources, 50% chance of success, 1/3 payoff to U.S.



Total value ~ \$296T at \$0.02 per kWhr thermal (\$FY2002)

Large CO2 Emissions cuts needed to stabilize CO2 & associated global warming



^{*} Kyoto Accords: 2012 target 10% below 1990

GWH: Adequate reductions in CO2 over next 50 years probably possible with improved efficiency, windmills, fission, CO2 sequestration, etc. But after 50 years, need fusion, or fission breeders, or ??

Future Gen Flow Diagram



2004 National AFV Day Odyssey - West Virginia / GJS / April 2, 2004

From Gary J. Stiegel, http://wvodyssey.nrcce.wvu.edu/2004/post_event/ppt/Stiegel_gasification.ppt

A Crash Course in Magnetic Confinement (in 3 slides)







poloidal projection

Perspective view

The Most Successful Magnetic Confinement Configuration is the Tokamak



 \downarrow turbulence & $\uparrow\beta$ could significantly improve fusion



From Galambos, Perkins, Haney, & Mandrekas 1995 Nucl.Fus. (very good), scaled to match ARIES-AT reactor design study (2001), http://aries.ucsd.edu/ARIES/

 \downarrow turbulence & $\uparrow \beta$ could significantly improve fusion



FIG. 4. Minimum COE steady state reactor parameters versus the net electric output. Cases are shown for three physics levels: (a) present day levels that would be sustainable in a non-transient manner in a conservatively designed system (H $\leq 2, \beta_N \leq 2.5$), (b) moderately improved physics (H $\leq 3, \beta_N \leq 4$) and (c) advanced physics (H $\leq 4, \beta_N \leq 6$).

Table 1: Major Parameters of ARIES-AT

4.0
5.2
1.3
2.2
0.84
5.4*
9.2 %
2.3
2.4
1.4
13
36
6.0
11.4
59%
3.3
1,755
14%
51%
5





Figure 1.2.1-2 ITER Tokamak Cutaway

Parameter	400 MW	500 MW
R/a (m/m)	6.2/2.0	6.2/2.0
Volume (m ³)	831	831
Surface (m ²)	683	683
Sep.length (m)	18.2	18.2
S _{cross-sect.} (m ²)	21.9	21.9
B_T (T)	5.3	5.3
I _P (MA)	15.0	15.0
κ_X / δ_X	1.85/0.48	1.85/0.48
κ 95/δ95	1.70/0.33	1.70/0.33
$l_i(3)$	0.84	0.84
V _{loop} (mV)	75	75
q ₉₅	3	3
$\beta_{\rm N}$	1.8	2.0
$< n_e > (10^{19} \text{ m}^{-3})$	10.1	11.3
<ne>/nG</ne>	0.85	0.94
<t<sub>e> (keV)</t<sub>	8.8	8.9
$< T_i > (keV)$	8.0	8.1
$<\!\!\beta_{\mathrm{T}}\!\!>$ (%)	2.5	2.8
β_{p}	0.65	0.72
ΓP		••••=
Parameter	400 MW	500 MW
Parameter P _{RF} + P _{NB} (MW)	400 MW	500 MW
$\label{eq:product} \begin{array}{c} \textbf{Parameter} \\ P_{RF} + P_{NB} \left(MW \right) \\ P_{OH} (MW) \\ P_{TOT} (MW) \end{array}$	400 MW 7 + 33	500 MW 17 + 33
$\begin{tabular}{l} \hline Parameter \\ \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} (MW) \end{tabular}$	400 MW 7 + 33 1 121 21	500 MW 17 + 33 1 151 26
ParameterP _{RF} + P _{NB} (MW)P _{OH} (MW)P _{TOT} (MW)P _{BRM} (MW)P _{SYN} (MW)	400 MW 7+33 1 121 21 8	500 MW 17 + 33 1 151 26 8
ParameterP _{RF} + P _{NB} (MW)P _{OH} (MW)P _{TOT} (MW)P _{BRM} (MW)P _{SYN} (MW)P _{LINE} (MW)	400 MW 7 + 33 1 121 21 8 18	500 MW 17 + 33 1 151 26 8 27
$\begin{tabular}{lllllllllllllllllllllllllllllllllll$	400 MW 7 + 33 1 121 21 8 18 47	500 MW 17 + 33 1 151 26 8 27 61
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$\begin{tabular}{lllllllllllllllllllllllllllllllllll$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48	500 MW 17 + 33 1 151 26 8 27 61 500 104/51
$\begin{tabular}{lllllllllllllllllllllllllllllllllll$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10
$\begin{tabular}{ c c c c } \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{BRM} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{FUS} & (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline \tau_E & (s) \\ \hline \end{tabular}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4
$\begin{tabular}{ c c c c } \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{BRM} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{FUS} & (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline τ_E & (S) \\ \hline W_{th} & (MJ) \\ \hline \end{tabular}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353
$\begin{tabular}{ c c c c } \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{BRM} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{FUS} & (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline \tau_E & (s) \\ \hline \end{tabular}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320 32	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353 34
$\begin{tabular}{ c c c c } \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{BRM} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline τ_E & (s) \\ \hline τ_E & (s) \\ \hline w_{th} & (MJ) \\ \hline W_{fast} & (MJ) \\ \hline $H_{H98} (y,2) \\ \hline \end{tabular}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320 32 1.0	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353 34 1.0
$\begin{array}{c} \label{eq:product} P_{RF} + P_{NB} (MW) \\ P_{OH} (MW) \\ P_{TOT} (MW) \\ P_{TOT} (MW) \\ P_{BRM} (MW) \\ P_{SYN} (MW) \\ P_{LINE} (MW) \\ P_{LINE} (MW) \\ P_{RAD} (MW) \\ P_{FUS} (MW) \\ P_{FUS} (MW) \\ P_{LOSS} / P_{L-H} \\ Q \\ \hline \tau_E (s) \\ W_{th} (MJ) \\ W_{fast} (MJ) \\ H_{H98}_{(y,2)} \\ \hline \tau_{He}^{*} / \tau_{E} \\ \end{array}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320 32 1.0 5	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353 34 1.0 5
$\begin{array}{c} \textbf{Parameter} \\ \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} (MW) \\ \hline P_{TOT} (MW) \\ \hline P_{TOT} (MW) \\ \hline P_{BRM} (MW) \\ \hline P_{SYN} (MW) \\ \hline P_{LINE} (MW) \\ \hline P_{LINE} (MW) \\ \hline P_{RAD} (MW) \\ \hline P_{RAD} (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline \tau_E (s) \\ \hline W_{th} (MJ) \\ \hline W_{fast} (MJ) \\ \hline H_{H98 (y,2)} \\ \hline \tau_{He} / \tau_E \\ \hline Z_{eff, ave} \\ \end{array}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320 32 1.0 5 1.66	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353 34 1.0 5 1.72
$\label{eq:product} \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} (MW) \\ \hline P_{TOT} (MW) \\ \hline P_{TOT} (MW) \\ \hline P_{BRM} (MW) \\ \hline P_{SYN} (MW) \\ \hline P_{LINE} (MW) \\ \hline P_{LINE} (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline \tau_E (S) \\ \hline W_{th} (MJ) \\ \hline W_{fast} (MJ) \\ \hline H_{H98} (y,2) \\ \hline \tau_{He} / \tau_E \\ \hline Z_{eff, ave} \\ \hline f_{He,axis / ave} (\%) \\ \hline \end{array}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320 32 1.0 5 1.66 4.3/3.2	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353 34 1.0 5 1.72 4.4/3.2
$\begin{tabular}{ c c c c c } \hline P_{RF} + P_{NB} (MW) \\ \hline P_{OH} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{TOT} & (MW) \\ \hline P_{BRM} & (MW) \\ \hline P_{SYN} & (MW) \\ \hline P_{LINE} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{RAD} & (MW) \\ \hline P_{FUS} & (MW) \\ \hline P_{LOSS} / P_{L-H} \\ \hline Q \\ \hline \tau_E & (s) \\ \hline W_{th} & (MJ) \\ \hline W_{fast} & (MJ) \\ \hline H_{H98 (y,2)} \\ \hline \tau_{He}^{*} / \tau_E \\ \hline Z_{eff, ave} \\ \hline \end{tabular}$	400 MW 7 + 33 1 121 21 8 18 47 400 87/48 10 3.7 320 32 1.0 5 1.66	500 MW 17 + 33 1 151 26 8 27 61 500 104/51 10 3.4 353 34 1.0 5 1.72

Stronger plasma shaping improves performance



Confinement degrades if density too large relative to empirical Greenwald density limit $n_{Gr} = I_p /(\pi a^2)$, but improves with higher triangularity.

Compared to original 1996 ITER design, new ITER-FEAT 2001 and FIRE designs can operate at significantly lower density relative to Greenwald limit, in part because of higher triangularity and elongation.

Improved new fusion designs \downarrow uncertainties

Density and pressure limits improve with elongation κ & triangularity δ :

Empirical Greenwald density limit

$$\mu \text{ limit} \qquad n_{Gr} = \frac{I_p}{\pi a^2} \propto \frac{B_T}{Rq_{95}} \left[1 + \kappa^2 \left(1 + 2\delta^2 \right) \right]$$
$$\beta = \frac{p}{B^2 / 8\pi} \propto \frac{I_p}{aB_T} \propto \frac{a}{Rq_{95}} \left[1 + \kappa^2 \left(1 + 2\delta^2 \right) \right]$$

Pressure limit

New ITER-FEAT design uses segmented central solenoid to increase shaping.

FIRE pushes to even stronger shaping (feedback coils closer) & reduced size with high field cryogenic CuBe (achievable someday with high-Tc superconductors?)

	R (m)	a (m)	В (T)	l _p (MA)	n _{Gr} 10 ²⁰ /m ³	<n<sub>e> /n_{Gr}</n<sub>	κ _χ	δ _x	P _{fusion} MW	Ρ _α /2πR	τ _Ε / τ _{98Η}	β_{norm}
ITER-96	8.14	2.80	5.68	21.0	0.85	1.50	1.75	0.35	1500	5.9		
ITER-FEAT	6.20	2.00	5.30	15.1	1.19	0.85	1.85	0.48	400	2.0	1.0	1.8
FIRE	2.14	0.60	10.0	7.7	6.92	0.66	2.00	0.70	150	2.2	1.0	1.8
Aries-AT	5.20	1.30	5.86	12.8	2.41	1.00	2.18	0.84	1760	9.0	1.4	5.4

Caveats: remaining uncertainties regarding confinement, edge pedestal scaling, ELMs, disruptions & heat loads, tritium retention, neoclassical beta limits, but also good ideas for fixing potential problems or further improving performance.

MFE CONFIGURATIONS IN THE PORTFOLIO

Externally Controlled



Example: Stellarator

Coils link plasma Magnetic fields from external currents Toroidal field >> poloidal field Large R/a More stable, better confinement



Self Organized

Example: FRC

Coils do not link plasma B from internal currents Poloidal B >> Toroidal B R/a \rightarrow 1.0 Higher power density
Next few slides: Intuitive picture of the toroidal plasma instabilities, and how to stabilize them

-- based on analogy with Inverted pendulum / Rayleigh-Taylor instability



"Bad Curvature" instability in plasmas ≈ Inverted Pendulum / Rayleigh-Taylor Instability

Growth rate:

Top view of toroidal plasma:



Twist in **B** carries plasma from bad curvature region to good curvature region:



Similar to how twirling a honey dipper can prevent honey from dripping.

Spherical Torus has improved confinement and pressure limits (but less room in center for coils)



Tokamak

Improved Stellarators Being Built

- Magnetic field twist and shear provided by external coils, not plasma currents. More stable?
- Computer optimized designs much better than 1950-60 slide rules?
- Quasi-toroidal symmetry allows plasma to spin toroidally: shear flow stabilization?





These physical mechanisms can be seen in gyrokinetic simulations and movies

particles quickly move along field lines, so density perturbations are very extended along fields lines, which twist to connect unstable to stable side

Stable

smaller

eddies

side,

Unstable bad-curvature

side, eddies point out,

direction of effective

gravity

Movie http://fusion.gat.com/theory/Gyromovies shows contour plots of density fluctuations in a cut-away view of a GYRO simulation (Candy & Waltz, GA). This movie illustrates the physical mechanisms described in the last few slides. It also illustrates the important effect of sheared flows in breaking up and limiting the turbulent eddies. Long-wavelength equilibrium sheared flows in this case are driven primarily by external toroidal beam injection. (The movie is made in the frame of reference rotating with the plasma in the middle of the simulation. Barber pole effect makes the dominantly-toroidal rotation appear poloidal..) Short-wavelength, turbulent-driven flows also play important role in nonlinear saturation.



The electrostatic Gyrokinetic equation, in a Drift-Kinetic-like form for the full, gyro-averaged, guiding center density $\bar{f}(\vec{R}, v_{\parallel}, \mu, t)$:

$$\frac{\partial \overline{f}}{\partial t} + (v_{\parallel} \hat{\mathbf{b}} + \mathbf{v}_{E} + \mathbf{v}_{d}) \cdot \nabla \overline{f} + \left(\frac{q}{m} E_{\parallel} - \mu \nabla_{\parallel} B + v_{\parallel} (\hat{\mathbf{b}} \cdot \nabla \hat{\mathbf{b}}) \cdot \mathbf{v}_{E}\right) \frac{\partial \overline{f}}{\partial v_{\parallel}} = 0$$

$$\underbrace{\bigvee_{E}}_{VE} = -\underbrace{c}_{B} \nabla \langle \overline{E} \rangle \times \widehat{b} \qquad E_{\parallel} = -\widehat{b} \cdot \nabla \langle \overline{E} \rangle \qquad \mu^{=-\frac{1}{2}} \frac{v_{\perp}^{2}}{B}$$

$$\underbrace{vsing}_{VJ} gyro averaged \text{ potential } \langle \overline{\Phi} \rangle (\overline{R}) = \frac{1}{2\pi} \int d\theta \ \overline{\Phi} (R + \rho(\theta))$$

$$\underbrace{\bigvee_{J}}_{VJ} = \nabla B + curvature \qquad h^{-1} \nabla_{\theta} (h_{\perp} \rho) \ \overline{\Phi}_{h} e^{ihR}$$

$$\underbrace{\overline{\Phi} (\chi)}_{R} \qquad \underbrace{\overline{\Phi} (\chi)}_{R} \qquad \chi$$

2. Development of & physics in gyrokinetic equations

if low frequencies $\omega \ll$ cyclotron frequency (Ω_c) , \rightarrow average over particle gyration, treat particles as rings of charge in spatially varying fields



 $E \times B \to -\nabla \langle \Phi \rangle \times \vec{B}$

potential averaged around particle orbit, even if $k_{\perp}\rho_i$ large



When calculating charge at point Q, have to sum over all particles whose guiding centers are on the dashed line, & have to include small variation of particle density around gyro-orbit (\rightarrow polarization shielding)

Development of nonlinear gyrokinetics was a major breakthrough

3. Fairly Comprehensive 5-D Gyrokinetic Turbulence Codes Have Been Developed



- Solve for the particle distribution function $f(r, \alpha, \theta, E, \mu, t)$ (avg. over gyration: 6D \rightarrow 5D)
 - 500 radii x 32 complex toroidal modes (96 binormal grid points) x 10 parallel points along half-orbits x 8 energies x 16 v_{||}/v 12 hours on ORNL Cray X1E with 256 MSPs
- Realistic toroidal geometry, kinetic ions & electrons, finite-β electro-magnetic fluctuations, collisions. Sophisticated algorithms.

Understanding Turbulence That Affects the Performance of Fusion Device



(Candy & Waltz, GA 2003)

Central temp ~ $10 \text{ keV} \sim 10^8 \text{ K}$

Large temperature gradient
→ turbulent eddies
→ cools plasmas
→ determines plasma size
needed for fusion ignition

Major progress in last decade: detailed nonlinear simulations (first 3-D fluid approximations, now 5-D f($\vec{x}, v_{\parallel}, v_{\perp}, t$)) & detailed understanding

Microinstabilities are small-amplitude but still nonlinear $n = n_o(r) + \tilde{n}(x,t)$ nor no >> ñ but $\nabla n_0 \sim \nabla \tilde{n}$ Can locally flatten or reverse total gradient that was driving instability. * Turbulence causes loss of plasma to the wall, but confinement still × 105 better than without B. If no B_{2} , loss time ~ $\frac{q}{V_{+}}$ ~ 1 µsec with B, expts. measure ~ 0.1-1.0 sec.

Simple picture of reducing turbulence by negative magnetic shear

- Particles that produce an eddy tend to follow field lines.
- Reversed magnetic shear twists eddy in a short distance to point in the ``good curvature direction".
- Locally reversed magnetic shear naturally produced by squeezing magnetic fields at high plasma pressure: ``Second stability'' Advanced Tokamak or Spherical Torus.
- Shaping the plasma (elongation and triangularity) can also change local shear



Sheared flows can suppress or reduce turbulence



Carreras, Waltz, Hahm, Kolmogorov, et al.

Sheared ExB Flows can regulate or completely suppress turbulence (analogous to twisting honey on a fork)



Dominant nonlinear interaction between turbulent eddies and $\pm \theta$ -directed zonal flows.

Additional large scale sheared zonal flow (driven by beams, neoclassical) can completely suppress turbulence

Fascinating Diversity of Regimes in Fusion Plasmas. What Triggers Change? What Regulates Confinement?



Transition to Enhanced Confinement Regime is Correlated with Suppression of Core Fluctuations in TFTR



 Similar suppression observed on JET (X-mode reflectometer) and DIII-D (FIR Scattering)

Hahm, Burrell, Phys. Plas. 1995, E. Mazzucato et al., PRL 1996.



R. Nazikian et al.

All major tokamaks show turbulence can be suppressed w/ sheared flows & negative magnetic shear / Shafranov shift



Internal transport barrier forms when the flow shearing rate $dv_{\theta}/dr > \sim$ the max linear growth rate γ_{lin}^{max} of the instabilities that usually drive the turbulence.

Shafranov shift Δ ' effects (self-induced negative magnetic shear at high plasma pressure) also help reduce the linear growth rate.

Advanced Tokamak goal: Plasma pressure ~ x 2, $P_{fusion} \propto pressure^2 ~ x 4$

Impact of design changes in new ITER-FEAT.

- ITER-FEAT uses a segmented central solenoid which provides more shape control than the fixed central solenoid in the original 1996 ITER (some U.S. physicists/engineers had been pushing for this design change before the U.S. pulled out).
- Increased elongation κ_x from 1.75 to 1.85, triangularity δ_x from 0.34 to 0.48, reduced size from R=8.14 to 6.2 m. (FIRE would push each of these even further)

$$n_{Greenwald} = \frac{I_p}{\pi a^2} \propto \frac{B_t}{qR} \left[1 + \kappa^2 (1 + 2\delta^2) \right]$$

- At fixed $B_t \& q$, can increase Greenwald density limit (and current) by increasing $\kappa \& \delta$.
- Net effect: $n_{Greenwald}$ increased by 40% and $n_e/n_{Greenwald}$ dropped from 1.5 in ITER-96 to only 0.85 in ITER-FEAT (now accepted as a design rule maximum value for ITER-FEAT).
- When we started looking at these issues in 1995, some members of ITER central team said ITER had to work at this high density in order to not melt (or erode too quickly) the divertor.
- Rough measure of the divertor power load is P/R: 3 times lower in ITER-FEAT than ITER-96. Divertor plates have been inclined further. Now easier to handle lower density.
- By dropping nuclear testing requirement of P=1500 MW, Q can be increased by lowering power (until hitting H-mode power threshold), since if $\tau_E \sim P^{-2/3}$, then n T $\tau_E \sim P \tau_E^{-2} \sim P^{-1/3}$

More experience with advanced tokamak regimes.

- Advanced tokamak regimes with internal transport barriers (ITBs) might help to significantly improve tokamak confinement, beta limits, and power plant design (with higher self-driven bootstrap current).
- 1996/97 consensus expressed in 1997 FESAC review: advanced tokamak studies were very important, but were too new and uncertain for ITER to depend on.
- Further experience since then has been encouraging: internal transport barriers of various kinds achieved in largest tokamaks (incl. JET and JT-60U). These include electron transport barriers that apparently depend on high beta Shafranov shift effects and not on rotation (which might be harder to obtain at large reactor scales). Also have more experience sustaining them for longer times (DIII-D feedback expts.).
- Main mechanisms of ITBs qualitatively understood theoretically, but there are significant quantitative uncertainties in accessibility requirements. Nevertheless, experimental experience is encouraging that it may be possible.

Tokamak Turbulence Overview

- Motivation
- Simple physical pictures of tokamak plasma turbulence & how to reduce it (reversed magnetic shear, sheared flows, plasma shaping...)
- Simulation-based transport models (IFS-PPPL,...): stiff criticalgradient transport, sensitive to edge b.c.
- Worries about original ITER-96 design (problems with empirical fits, extreme density)
- Why recent designs are significantly better.
- Impressive progress with comprehensive 5-dimensional computer simulations being developed to understand plasma turbulence & optimize performance

Continuum/Eulerian Approach to Electromagnetic Gyrokinetic Turbulence

GS2 (Dorland & Kotschenreuther), GENE (Jenko), and GYRO (Candy & Waltz) have demonstrated that direct Eulerian simulations of microturbulence using the 5-D electromagnetic gyrokinetic equations can be effective, by

(1) Using modern massively parallel supercomputers and clusters, and

(2) Using modern advanced algorithms, including

- implicit / semi-implicit methods (or carefully designed explicit methods)
- pseudo-spectral and/or Arakawa treatment of nonlinearities (preserves all 3 conservation properties of Poisson bracket nonlinearities)
- pseudo-spectral and/or high-order upwind advection algorithms: very low dissipation at long wavelengths, effective sink at small scales.
- high-order velocity-space integration algorithms,
- efficient field-aligned coordinate systems, ...

Continuum/Eulerian Approach to Electromagnetic Gyrokinetic Turbulence

GS2 (Dorland & Kotschenreuther) http://gs2.sourceforge.net GENE (Jenko) http://www.ipp.mpg.de/~fsj/ GYRO (Candy & Waltz) http://fusion.gat.com/comp/parallel/

These codes widely used by many to study plasma turbulence in fusion devices. GYRO is currently the most comprehensive gyrokinetic code available:

- Gyrokinetic ions (multiple species) & adiabatic/drift-kinetic/gyrokinetic electrons
- Trapped and passing electrons (and ions) for Trapped Electron Mode
- Pitch-angle scattering collision operator (TEM / neoclassical effects)
- Finite beta magnetic fluctuations as well as electrostatic fluctuations (important for kinetic-ballooning modes, magnetic flutter contribution to transport)
- General shaped tokamak geometry
- Equilibrium ExB and parallel velocity shear
- Finite-p* effects (profile shear stabization, nonlocal transport)...

Nevertheless, a lot of interesting work remains to be done: more tests against experiments, particle transport, transport barrier formation, shaping effects, understand scalings, couple to transport codes for complete predictive ability, &:

edge simulations (new codes needed to do gyrokinetics in the edge, challenging...)

Comparison of GYRO Code & Experiment



- Gyrokinetic turbulence codes now including enough physics (realistic geometry, sheared flows, magnetic fluctuations, trapped electrons, fully electromagnetic fluctuations) to explain observed trends in thermal conductivity, in many regimes.
- Big improvement over 15 years ago, when there were x10 x100 disagreements between various analytic estimates of turbulence & expts.
- Now within experimental error on temperature gradient. Importance of critical gradient effects emphasized in 1995 gyrofluid-based IFS-PPPL transport model.
- Caveats: Remaining challenges: quantitative predictions of internal transport barriers, test wider range of parameters, & more complicated edge turbulence.

Largest GYRO simulations used to study interaction of ITG & ETG Turbulence

- 1280 $\rho_e \ge 1280 \rho_e \ge 20$ parallel pts/orbit ≥ 8 energies $\ge 16 v_{\parallel}/v$
- electrons + kinetic ions, $m_i/m_e = 20^2 30^2$
- 5 days on DOE/ORNL Cray X1E w/ 720 Multi-Streaming Processors



ETG + kinetic ion GYRO simulation movie

- large box on right: full simulation domain, 1280 $\rho_e x$ 1280 $\rho_e = 64 \rho_i x 64 \rho_i$
- small box on lower left: zoom in on a 64 ρ_e x 64 ρ_e patch

http://fusion.gat.com/THEORY/images/1/1f/ETG-ki.mpg from http://fusion.gat.com/theory/Gyromovies



ETG fluctuations ($k_{\perp}\rho_i > 1$) may account for significant fraction of transport in some plasmas

Simple scaling from ITG to ETG:

$$\begin{array}{l} \chi_{itg} ~\sim C_{itg} ~\rho_i^2 ~ v_{ti}/L \\ \chi_{etg} ~\sim C_{itg} ~\rho_e^2 ~ v_{te}/L ~\sim \chi_{itg} ~/60 \end{array}$$

But Dorland & Jenko (2000) showed ETG turbulence larger because:

perpendicular adiabatic ions for ETG gives more shielding of zonal electric fields than does parallel adiabatic electrons for ITG.

- Candy showed ETG will be reduced by kinetic ions, more so if strong ITG turbulence
- ITG can be weak near marginal stability w/ ExB shear. TGLF transport model shows ETG / high-k TEM may still be important in some cases.



J. Kinsey Bl2.6, Monday 12:00 Noon

TGLF exhibits lower average global errors than GLF23 for a large L- and H-mode profile database of 96 discharges

- Database: 25 DIII-D L-,33 DIII-D H-, 22 JET H-, 16 TFTR L-mode discharges
- Avg RMS errors in W_{inc} is 19% for TGLF, 36% for GLF23
- Avg RMS error in W_{tot} is ΔR_{Wtot} =10% for TGLF, 20% for GLF23





- 5. Future challenges & opportunities:
 - more detailed comparisons w/ expts incl. synthetic fluctuation diagnostics
 - coupling turbulence simulations directly in long-time transport codes
 - Edge Turbulence, very challenging but critical problem
 - Edge important: core depends on edge, ELMs, transport barriers
 - present core codes don't handle edge, need X-point separatrix, open & closed field lines, strong recycling, wide range of collisionality, ...



Simulated edge-plasma region



From Kinsey, Staebler, Waltz, Sherwood 2002. Predictions for 2001 ITER-FEAT.

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Selected Further References

- This talk: <u>http://fire.pppl.gov</u> & <u>http://w3.pppl.gov/~hammett</u>
- Plasma Microturbulence Project http://fusion.gat.com/theory/pmp
- GYRO code and movies <u>http://fusion.gat.com/comp/parallel/gyro.html</u>
- GS2 gyrokinetic code <u>http://gs2.sourceforge.net</u>
- My gyrofluid & gyrokinetic plasma turbulence references: <u>http://w3.pppl.gov/~hammett/papers/</u>
- "ENDING THE ENERGY STALEMATE: A Bipartisan Strategy to Meet America's Energy Challenges", The National Commission on Energy Policy, December 2004. http://www.energycommission.org/
- "Anomalous Transport Scaling in the DIII-D Tokamak Matched by Supercomputer Simulation", Candy & Waltz, Phys. Rev. Lett. 2003
- "Burning plasma projections using drift-wave transport models and scalings for the H-mode pedestal", Kinsey et al., Nucl. Fusion 2003
- "Electron Temperature Gradient Turbulence", Dorland, Jenko et al. Phys. Rev. Lett. 2000
- "Generation & Stability of Zonal Flows in Ion-Temperature-Gradient Mode Turbulence", Rogers, Dorland, Kotschenreuther, Phys. Rev. Lett. 2000
- "Comparisons and Physics Basis of Tokamak Transport Models and Turbulence Simulations", Dimits et al., Phys. Plasmas 2000.

Turbulence & Transport Issues Particularly Important in Burning plasmas

- Performance of burning plasma & fusion power plant very sensitive to confinement: potential significant improvements
- Uncertainties: Maintain good H-mode pedestal in larger machine at high density? ELM bursts not too big to avoid melting wall? Can internal transport barriers be achieved in large machine, for long times self-consistently with beta limits on pressure profiles and desired bootstrap current?
- Lots of progress in understanding turbulence in tokamaks, understand many pieces of the puzzle, but comprehensive tools for predicting and optimizing tokamaks remains to be developed...
- Highest priorities include need for developing comprehensive simulations of edge turbulence, extending the progress made in core gyrokinetics to the edge region to predict the temperature at the top of the pedestal, ELM size, H-mode power threshold...
- In present experiments, pressure profile can be controlled by external heating, currents primarily generated inductively. In a reactor, pressure and current profiles determined self-consistently from fusion heating and bootstrap currents. (Fortuitously, bootstrap currents give naturally hollow profiles, which gives favorable reversed magnetic shear.)
- Proposed Burning Plasma devices will pin down uncertainties in extrapolations: help design final power plant.